The California Central Valley Groundwater-Surface Water Simulation Model

#### Introduction

**CWEMF C2VSim Workshop** 

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### Outline

Geology and Geography

Historical and Current Water System

**Groundwater Studies & Models** 

**Integrated Water Flow Model** 

# California's Central Valley

- 20,000 sq. mi. (55,000 sq. km.)
- 30 MAF/yr Surface Water Inflow
- Agricultural Production
  - 6.8 million acres (27,500 sq. km)
  - <1% of US farm land
  - 10% of US crops value in 2002
- Population Growth
  - 1970: 2.9 million
  - 2005: 6.4 million
    - Groundwater Pumping
      - ~9 MAF in 2002
      - 10-18% if US pumping
      - Not measured or regulated

# Central Valley Hydrogeology

- Tectonic development
- Alluvial stratigraphy
- Geologic cross-section
- Groundwater studies & models

#### **Tectonic Development**



### 100 million years ago



#### Early Central Valley



#### **Tectonic Development**



#### **Tectonic Development**

CASCADIA SUBDUCTION ZONE – a nearly 700-mile long plate boundary where the Gorda and Juan de Fuca plates dive beneath the North American plate, extending from Cape Mendocino to Vancouver Island, Canada.

> COASTAL ONSHORE FAULTS - caused by the subduction of the Gorda plate. ...;

NORTH AMERICAN PLATE MODOC PLATEAU - a region of active volcanism and discontinuous faults.

of discontinuous active faults

MENDOCINO TRIPLE JUNCTION – the area where the Gorda, Pacific and North American plates meet, one of the most seismically active areas of the continental U.S.

PACIFICP

SAN ANDREAS FAULT SYSTEM – the 800-mile boundary between the Pacific and North American plate. The M 7.8 1906 earthquake ruptured 250 miles of the fault from Santa Cruz to Shelter Cove.

GORDA PLATE – plate offshore and beneath Northwestern California that is being crushed and faulted by plate motions to the north and south. Example: M 7.2, 1980; M 7.2, 2005.

JUAN DE FUCA

MENDOCINO FALLT – a 160-mile long plate boundary e, tending west from Cape Mendocino v here the Gorda and Pacific plates grine past one another. Example: M 7.0, 195 L





#### **Tectonic Subsidence**



### Central Valley Stratigraphy



#### Central Valley Stratigraphy



#### **Current Central Valley**

**Continental Deposits** 

**Marine Sediments** 

Crystalline Rocks (Coast Ranges) Crystalline Rocks (Sierra Nevada)



#### **River Fans**

**Continental Deposits** 

**Marine Sediments** 

Crystalline Rocks (Coast Ranges) Crystalline Rocks (Sierra Nevada)





Fig. 2. Schematic diagram of the Kings River alluvial fan and its geologic elements.

Harter et al. 2005.



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**Fig. 6.** Schematic cross-sections through: (**A**) the Kings River fluvial fan (based on Weissmann *et al.* 2002*a*, 2004); (**B**) the Tuolumne River fluvial fan (based on Burow *et al.* 2004); and (**C**) the Chowchilla River fluvial fan (based on Helley 1966).

Weissmann et al. 2005.

### Hydrogeology



#### **Corcoran Clay**



Buried remnant of a Pleistocene lake bed

Deposited 615,000 - 750,000 years ago

Deformed by tectonic subsidence



#### Land Surface Subsidence



#### Land Surface Subsidence



#### Land Surface Subsidence



#### **Groundwater Studies**



Bryan, 1923. Geology and ground-water resources of Sacramento Valley, California.

Mendenhall et al. 1916. Ground water in San Joaquin Valley, California.



#### **Groundwater Studies**



Olmsted and Davis. 1961. Geologic features and ground water storage capacity of the Sacramento Valley, California.

Davis et al. 1959. Ground-water conditions and storage capacity in the San Joaquin Valley California.



#### **Groundwater Studies**



Page. 1986. Geology of the fresh groundwater basin of the Central Valley, California.

> GEOLOGY OF THE FRESH GROUND-WATER BASIN OF THE CENTRAL VALLEY. CALIFORNIA, WITH TEXTURE MAPS AND SECTIONS





#### **Regional Models**

Williamson et al. 1989. Groundwater flow in the Central Valley, California.



JM Montgomery Engineers. 1990. California Central Valley Ground-Surface Water Model (CVGSM) Manual.



# **Regional Models**

Faunt et al. 2009. Groundwater availability of the Central Valley aquifer, California. DWR. 2012. California Central Valley Groundwater-Surface Water Simulation Model (C2VSim).





#### Faults

- Can act as flow barriers
- Several mapped on basement
- Vertical extent generally unknown



## Faults

- Battle Creek Fault
- Red Bluff Arch
- Plainfield Ridge
  Anticline
- Pittsburgh Kirby Hills – Vaca Fault
- Vernalis Fault
- Graveley Ford Faults
- Visalia Fault
- Pond-Poso Creek
  Fault
- Edison Fault
- White Wolf Fault



#### Aquifer Thickness

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#### Water Quality

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### History of Central Valley Water Development

#### 1800s

- Water development to support hydraulic mining
- Converted to irrigation after 1886
- Local diversions and irrigation canals within a watershed

Nady and Larragueta. 1983. Development of Irrigation in the Central Valley. USGS Hydrologic Atlas 649, plate 1.

### History of Central Valley Water Development

#### 1980

- Groundwater pumping
- Inter-basin Transfers
  - Hetch-Hetchy Aqueduct
  - Mokelumne Aqueduct
  - Central Valley Project
  - State Water Project

Nady and Larragueta. 1983. Development of Irrigation in the Central Valley. USGS Hydrologic Atlas 649, plate 2.


# **Climate Change**





**Decreasing California Snowpack** 

10% snowpack reduction 1960-2000.

Continued warming could reduce snowpack volume by 25% by 2050





## Integrated Water Flow Model (IWFM)

- Open-source, regional-scale integrated hydrologic model
- Simulates land surface, groundwater, surface water, and surface-groundwater interactions
- Represent agricultural and urban water management practices, and their effects on the water system



A planning and analysis tool that computes agricultural and urban water demands based on climatic, soil, land-use and agronomic parameters, then adjusts groundwater pumping and stream diversions to meet these demands

## **IWFM History**

### Derived from the Integrated Ground-Surface Water Model (IGSM)

- Originally developed by Young Yoon, UCLA (1976)
- Integrated model: Land Surface, Surface Water, Groundwater

### **Significant Models**

- Central Valley Ground-Surface Water Model (CVGSM)
- Salinas Valley Groundwater Basin model
- Western San Joaquin Valley (WESTSIM)
- Friant Service Area
- Yolo County IGSM Model
- Sacramento County IGSM Model
- North American River Basin Model
- Kings Groundwater Basin Model

## **IWFM History**

### **California Department of Water Resources**

- Required a Central Valley Model for CalSim3 development
- Acquired IGSM source code
- Peer review to identify strengths and weaknesses
- Comprehensive update, port to Object Oriented FORTRAN
- Release as open-source software
- Continued development and improvement

### Release

- Rename "Integrated Water Flow Model" in 2005
- Version 3.02 with subregional water budgets
- Version 4.0 with elemental water budgets



# Land Surface Process





# Surface Water Process







# **IWFM Small Watersheds**



# IWFM

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# **IWFM Water Balance Diagram**

## Simulated Annual Water Budget

Average Flows for water years 2000-2009 [Million Acre-Feet/Year]



## **Object-Oriented Design**



## Link with Other Models



# **IWFM** Application

IWFM consists four programs executed in sequence



# **IWFM Pre-Processor**

Pre-processor

- Read nodal coordinates
- Link nodes to form elements
- Compile vertical aquifer stratigraphy at each node
- Link selected nodes to form river reaches
- Link river reaches into a flow network
- Compile profiles for river nodes
- Apply soil properties to elements
- Apply drainage patterns to elements
- Assign elements to subregions
- Link precipitation data to elements
- Compile specified pumping wells

# **IWFM** Simulation

### Simulation

- Read binary file produced by Preprocessor
- Calculate a balanced water budget for each model component for each time step
  - Precipitation, river inflow, diversions
  - Land use, crop acreage \* ET, urban demands
  - Runoff and return flow
  - Deep percolation
  - Stream-groundwater flows
  - Calculate groundwater pumping
- Write out results for each time step to a series of files:
  - Budget and Z-Budget results to binary files
  - Groundwater and surface water hydrographs to text files
  - TecPlot movie data to text files

# **Simulation Scheme**



# **IWFM Post-Processors**

Post-processors (Budget, Z-Budget)

- Read binary files produced by Simulation
- Budget tabulates a set of water budgets:
  - Land and Water Use
  - Root Zone
  - Groundwater
  - Stream Reaches
  - Small-Stream Watersheds
- Z-Budget compiles water budgets for user-specified aquifer zones of one to many elements. Example zones:
  - Subregions
  - Hydrologic Regions
  - Groundwater Basins

# Input and Output Files

- <u>Input files</u> contain comment fields
- Tab-delimited for easy cut-and-paste with Excel
- Time-tracking simulations are aware of the date and time; <u>input and output</u> <u>time-series data</u> have a date and time stamp

C*************************************
C C NRAIN : Number of rainfall stations (or pathnames if DSS files are used)
C used in the model
FACIRN; Conversion factor for rainfall rate It is used to convert only the spatial component of the unit;
DO NOT include the conversion factor for time component of the unit.
* e.g. Unit of rainfall rate listed in this file = INCHES/MONIH Consistent unit used in simulation = FEET/DAY
Enter FACTRN (INCHES/MONTH -> FEET/MONTH) = 8.33333E-02
NSPRN ; Number of time steps to update the precipitation data
* Enter any number if time-tracking option is on
* Enter 0 if full time series data is supplied
* Enter any number if time-tracking option is on DSSFL · The name of the DSS file for data input (maximum 50 characters)
* Leave blank if DSS file is not used for data input
VALUE DESCRIPTION
1602 / NRAIN
U.U8333 / FACTRN (in/month -> ft/month) 1 / NSPRN
0 / NFQRN
/ DS3rL
Rainfall Data (PEAD FROM THIS FILE)
List the rainfall rates for each of the rainfall station below, if it will not be read from a DSS file (i.e. DSSFL is left blank above).
ITDN Time
ARAIN; Rainfall rate at the corresponding rainfall station; $[L/T]$
ITRN ARAIN(1) ARAIN(2) ARAIN(3)
Time 1 2 3 4 5 6 7 8
0/31/1921_24:00 1.34 1.34 1.32 1.27 1.34 1.31 1.30 1.34 1/30/1921_24:00 3.64 3.62 3.59 3.49 3.62 3.51 3.56 3.62
2/31/1921_24:00 8.15 8.14 7.86 7.49 8.08 7.43 8.01 7.97
L/31/1922_24:00 1.32 1.46 1.62 1.80 1.22 1.40 1.27 1.11 2/28/1922_24:00 7.61 7.95 7.98 8.02 7.25 7.23 7.09 6.63
3/31/1922_24:00 4.33 4.39 4.31 4.28 4.22 4.03 4.09 4.06
4/30/1922_24:00 0.94 0.91 0.92 0.91 0.94 0.93 0.93 0.94 5/31/1922_24:00 2.20 2.18 2.18 2.09 2.22 2.19 2.18 2.26
6/30/1922_24:00 0.71 0.72 0.67 0.62 0.76 0.58 0.74 0.82
//31/1922_24:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
9/30/1922_24:00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
.u/31/1922_24:uu 3.44 3.45 3.39 3.23 3.42 3.28 3.39 3.40 .1/30/1922_24:u0 3.54 3.64 3.74 3.79 3.47 3.51 3.41 3.22
2/31/1922_24:00 8.44 8.84 8.63 8.94 8.22 8.27 8.01 7.75
11/31/1923_24:00 4.06 4.09 4.02 3.90 4.05 3.95 3.99 4.01 02/20/1923_24.00 1.14 1.14 1.24 1.22 1.11 1.11 1.12 1.00



# Suggested File Hierarchy



# **Detailed Budget Tables**

					GRO	UND WATER BUDGE	IWFM (v3.02.00 ET IN AC.FT. FC AREA: 328277.0	)36) DR SUBREGION 1 58 AC	1 (DSA 58)	
 Time	Deep Percolation	Beginning Storage (+)	Ending Storage (-)	Net Deep Percolation (+)	Gain from Stream (+)	Recharge (+)	Gain from Lake (+)	Boundary Inflow (+)	Subsidence (+)	Subsurface Irrigatior (+)
10/31/1921_24:00	0.0	41093269.2	40825799.7	80152.5	-364317.1	867.7	0.0	5580.5	69.3	0.0
12/21/1921_24:00	1774 9	40825799.7 10707500 0	40/8/589.3 10701710 0	46959.9 22677 E	-102230.7	58.4 1 C	0.0	5526.1 6172 2	41.7 27 E	0.0
$12/31/1921_24.00$	187 2	40781748 8	40701740.0	24643 6	-52693 1	1.5	0.0	6281 5	19.9	0.0
02/28/1922 24:00	969.5	40770213.1	40770676.2	19687.5	-37994.6	1.2	0.0	8451.2	10.2	0.0
03/31/1922_24:00	34.8	40770676.2	40763511.0	16261.0	-41925.0	1.4	0.0	8745.3	9.1	0.0
04/30/1922_24:00	2196.2	40763511.0	40755221.4	13895.3	-39956.6	837.8	0.0	8377.2	7.3	0.0
05/31/1922_24:00	8993.9	40755221.4	40740684.9	12612.7	-46117.7	1645.9	0.0	8295.0	6.2	0.0
06/30/1922_24:00	10397.7	40740684.9	40716832.4	12115.7	-55090.5	2113.2	0.0	8213.7	8.5	0.0
07/31/1922_24:00	12958.4	40716832.4	40696603.9	12348.8	-51668.9	2579.8	0.0	8013.1	6.3	0.0
08/31/1922_24:00	14326.9	40696603.9	40680/95.6 40445417 5	12962.9	-4/632.8	2563.0	0.0	/933.4 7054 4	5.0	0.0
10/31/1922 24:00	5271.0	40660795.6	40665417.5	11835 0	-43693.0	829 1	0.0	7034.4	4.7	0.0
11/30/1922 24:00	478 3	40650780 5	40636197 5	10724 0	-40814 8	1 3	0.0	7819 7	14 7	0.0
12/31/1922 24:00	1856.0	40636197.5	40631348.0	9674.8	-31697.4	1.5	0.0	9430.8	10.7	0.0
01/31/1923_24:00	1198.6	40631348.0	40621470.3	8846.1	-36887.5	1.4	0.0	10470.0	11.3	0.0
02/28/1923_24:00	0.0	40621470.3	40604148.5	8079.5	-43167.9	1.2	0.0	10158.4	12.0	0.0
03/31/1923_24:00	0.0	40604148.5	40588048.2	7412.7	-40767.2	44.8	0.0	10058.5	11.6	0.0
04/30/1923_24:00	1834.1	40588048.2	40580201.5	6917.9	-32751.9	700.1	0.0	10333.0	9.2	0.0
05/31/1923_24:00	8555.3	40580201.5	40556339.0	6935.8	-49348.2	1703.0	U.U	9949.2	13.9	U.U
07/21/1922 24:00	10818.1	40556339.0 ADE24626 A	40534626.4	7422.6 0450.6	-4/830.2	2070.6	0.0	9851.4	13.8	0.0
07/31/1923_24.00	14467 1	40534626.4 10515163 6	40313103.0	0437.0 9897 N	-40713.9	2077.4 2559.9	0.0	7034.0 9538 8	14 2	0.0
00/31/1923 - 24.000	10163 2	40313103.0	40499071.0	10552 6	-42589 2	1666 5	0.0	9563 9	19.0	0.0
10/31/1923 24:00	0.0	40484602.6	40468059.3	9538.2	-41652.2	64.4	0.0	9469.9	19.6	0.0
11/30/1923_24:00	0.0	40468059.3	40450811.5	8501.7	-40492.9	53.9	0.0	9376.9	19.8	0.0
12/31/1923_24:00	0.0	40450811.5	40436600.4	7669.7	-37125.4	1.5	0.0	9284.8	17.8	0.0
01/31/1924_24:00	603.7	40436600.4	40422598.1	6936.0	-36112.1	1.4	0.0	9264.8	16.8	0.0
02/29/1924_24:00	421.4	40422598.1	40411736.8	6346.5	-33109.2	1.2	U.U	9932.6	15.6	U.U
03/31/1924_24:00	4170 5	40411/35.8	40392170.2	5843.5	-405/2.7	18.9	0.0	9636.3	18.3	U.U 0 0
04/30/1924_24:00	41/2.5 5909 3	40372170.2	40372004.1 10355592 5	5560.2	-37141.0	1115.0	0.0	7460.1 9324 2	15.0	0.0
06/30/1924 24:00	7155 9	40372004.1	40338481 8	5723 5	-39233 5	1811 4	0.0	9231 4	17 1	0.0
07/31/1924 24:00	8853.1	40338481.8	40322659.5	6144.1	-38418.7	2109.8	Ŭ.Ŭ	9139.6	16.6	Ŭ.Ŭ
08/31/1924_24:00	9954.3	40322659.5	40308146.4	6804.5	-37605.7	2030.9	0.0	9053.6	16.0	0.0
09/30/1924_24:00	10544.7	40308146.4	40294384.2	7623.4	-37206.8	1921.5	0.0	8958.7	15.6	0.0
10/31/1924_24:00	5726.2	40294384.2	40286744.8	7853.9	-30520.4	829.1	0.0	9234.7	13.0	0.0
11/30/1924_24:00	811.0	40286744.8	40280979.5	7421.2	-27505.9	1.4	0.0	9341.1	11.6	0.0
12/31/1924_24:00	1522.4	40280979.5	40277307.1	6906.2	-26190.0	1.6	U.U	10544.1	10.0	U.U
02/20/1925_24:00	0/5.5	40277307.1	40272288.2	6382.7 E929 7	-27490.1	1.4	0.0	12000 1	5.5	0.0
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0.03/31/1925 - 24.00	1228.9	40276792 9	40272302 1	5129 9	-26339 4	174 3	0.0	14141 7	11 2	0.0
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06/30/1925_24:00	10936.7	40256625.0	40238249.9	5803.6	-44772.6	2097.3	0.0	13575.9	14.2	0.0
07/31/1925_24:00	13349.6	40238249.9	40223940.3	6609.8	-41601.2	2567.0	0.0	13322.1	13.4	0.0
08/31/1925_24:00	14753.1	40223940.3	40214408.3	8070.7	-38148.7	2548.5	0.0	13189.6	11.9	0.0
09/30/1925_24:00	14694.2	40214408.3	40207991.2	9669.7	-36047.1	2225.4	0.0	13178.5	10.8	0.0
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	Time	Percolation	Storage (+)	(-)	Percolation	Stream (+)	(+)	Lake (+)	Inflow (+)	(+)	Irrigat
5			2 ( )		(+)						(+)
6	10/31/1921 12:00 AM	107,891.70	3,102,558,944.94	3,101,455,762.76	1,545,662.5	5 -1,380,216.55	1,027,128.06	-1,807,079.49	31,090.13	90,405.00	
7	11/30/1921 12:00 AM	10,499.60	3,101,455,762.76	3,101,687,810.88	922,094.9	7 -853,966.91	254,904.92	-78,310.97	36,201.50	56,617.07	
8	12/31/1921 12:00 AM	388,957.48	3,101,687,810.88	3,102,682,423.77	741,696.2	2 -216,993.75	346,284.30	17,852.75	72,838.18	39,597.99	
9	01/31/1922 12:00 AM	288,004.05	3,102,682,423.77	3,103,133,215.27	599,366.2	4 -560,369.70	313,857.01	18,954.57	59,790.60	34,261.40	
10	02/28/1922 12:00 AM	459,924.77	3,103,133,215.27	3,104,249,438.91	598,605.7	9 15,574.91	396,432.61	12,344.91	77,750.28	27,915.73	
11	03/31/1922 12:00 AM	79,849.93	3,104,249,438.91	3,104,396,762.34	433,088.5	2 -505,423.51	272,187.24	1,602.94	67,726.33	36,638.00	
12	04/30/1922 12:00 AM	111,986.03	3,104,396,762.34	3,104,289,059.02	386,101.0	8 -297,765.27	240,572.35	-5,210.40	41,927.63	37,081.13	
13	05/31/1922 12:00 AM	300,406.95	3,104,289,059.02	3,105,144,811.92	398,053.8	2 94,041.18	609,448.05	-14,825.96	44,015.81	29,131.90	
14	06/30/1922 12:00 AM	295,835.03	3,105,144,811.92	3,105,311,640.26	398,037.3	8 -465,298.77	618,372.60	-16,319.23	38,869.57	48,762.12	
15	07/31/1922 12:00 AM	117,767.33	3,105,311,640.26	3,104,218,749.41	320,944.8	0 -998,822.49	287,627.18	-12,155.49	37,650.36	77,713.66	
16	08/31/1922 12:00 AM	83,349.87	3,104,218,749.41	3,103,179,917.61	287,975.7	0 -764,044.06	201,662.00	-9,568.70	37,245.50	80,870.22	
17	09/30/1922 12:00 AM	28,923.90	3,103,179,917.61	3,102,820,892.90	253,924.3	3 -596,841.42	149,685.52	-7,595.87	36,845.29	23,265.59	
18	10/31/1922 12:00 AM	10,428.49	3,102,820,892.90	3,102,582,016.85	225,377.2	0 -452,920.73	127,476.29	-4,115.57	43,394.52	24,244.99	
19	11/30/1922 12:00 AM	70,374.76	3,102,582,016.85	3,102,721,899.87	222,037.8	7 -270,795.03	140,477.99	-1,732.60	50,286.94	12,802.53	
20	12/31/1922 12:00 AM	533,756.17	3,102,721,899.87	3,103,584,673.76	345,057.0	0 170,966.55	267,785.60	1,642.19	74,722.35	9,683.82	
21	01/31/1923 12:00 AM	261,607.92	3,103,584,673.76	3,103,741,171.42	315,762.4	7 -394,511.54	202,499.85	-/44./6	59,740.68	11,617.37	
22	02/28/1923 12:00 AM	9,367.59	3,103,741,171.42	3,103,658,892.63	223,091.5	9 -505,579.67	181,794.97	-1,683.15	47,251.54	11,187.23	
23	03/31/1923 12:00 AM	44,164.47	3,103,658,892.63	3,103,171,074.82	201,887.7	5 -412,750.01	165,605.02	-3,402.00	41,247.75	44,107.47	
24	04/30/1923 12:00 AM	233,033.44	3,103,171,074.82	3,103,587,456.36	232,389.7	i δ0,022.76	291,007.94	-0,032.68	10,155.39	13,045.71	
20	06/20/1022 12:00 AM	330,240.90	3,103,587,450.30	3,103,004,048.83	201,007.7	0 -223,711.09 8 527.062.02	300,400.74	-10,428.24	40,000.98	33,112.55	
20	00/30/1923 12:00 AM	200,100.02	3,103,004,048.83	3 102,091,317.94	221 507 4	-527,002.02 4 571.01/ 22	201,900.07	-10,000.77	30 /72 15	95.039.04	
20	09/21/1022 12:00 AM	90 967 15	3 101 006 265 57	3 101 030 102 00	221,007.4	0/1,914.00 6 566 972 00	169 454 00	-13,201.10	30,472.10	84 120 00	
20	09/30/1923 12:00 AM	40 347 40	3 101 039 102 09	3 100 856 489 57	186 652 1	9 -421 756 00	126 753 62	-11,201.00	45 086 41	11 231 72	
30	10/31/1923 12:00 AM	10 213 68	3 100 856 488 57	3 100 591 491 95	165 245 1	6 _337 797 06	104 846 44	-5 843 04	40,668,26	20.628.35	
31	11/30/1923 12:00 AM	8 320 47	3 100 591 491 95	3 100 474 310 43	151 010 1	6 -372 397 35	92 894 94	-3 338 63	38 773 25	7 927 13	
22	10/01/1020 12:00 AM	10 612 22	2 100 474 210 42	2 100 421 642 41	101,010.10	0 017 74 <u>0 07</u>	02,004.04	1 706 60	11 501 60	6 050 16	
14 4	Subregion 19 (DS/	A 60F) 🔬 Subre	gion 20 (DSA 60G)	Subregion 21 (DSA 60H)	Subregion	22 (ENTIRE M 4					
Rea	dy 🛅									U U	. 🕀

# **HEC-DSS**

VSim_R365.D55 - HEC-D55Vue Edit View Display Utilities	Help					
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ile <u>Name:</u> Z:\temp\r365\1921-20 athnames Shown: 4204 Pathnam	09-DSS\Results\C2VSim_F les Selected: 0 Pathnames	365.DSS : in File: 37836 File :	Size: 33987 KB			
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y Parts: B: WVFM DIVERDTL E	BUD	🗐 D:		E E		
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umber IWFM_L&W_USE B	UD	Cpart	D part / range	E part	F part	
1 MENIWEM LAKE BUD		VOLUME	01JAN1920 - 01JAN2000	1MON	DELI	
2 MENIWEM BOOTZN BL	חו	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI_SHORT	
3 MAEN STREAM BU		VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER	
		VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER_SHORT	
	100	- VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER	
6 WVFN_SVVSHED_BU			01JAN1920 - 01JAN2000	1MON	DIVER_SHORT	
7 WFM_DIVERDTL_BUD	SR10:DV130:R134	VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER	
8 WVFM_DIVERDTL_BUD	SR10:DV130:R134	VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER_SHORT	
9 WFM_DIVERDTL_BUD	SR10:DV131:R115	VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER	
10 WFM_DIVERDTL_BUD	SR10:DV131:R115	VOLUME	01JAN1920 - 01JAN2000	1MON	DIVER_SHORT	
11 WFM_DIVERDTL_BUD	SR10:DV172:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI	
12 WFM_DIVERDTL_BUD	SR10:DV172:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI_SHORT	
13 WVFM_DIVERDTL_BUD	SR10:DV173:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI	
14 WVFM_DIVERDTL_BUD	SR10:DV173:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI_SHORT	
15 WVFM_DIVERDTL_BUD	SR10:DV174:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI	
16 WFM_DIVERDTL_BUD	SR10:DV174:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI_SHORT	
17 WVFM_DIVERDTL_BUD	SR10:DV176:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI	
18 WFM_DIVERDTL_BUD	SR10:DV176:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI_SHORT	
19 WFM_DIVERDTL_BUD	SR10:DV177:R0	VOLUME	01JAN1920 - 01JAN2000	1MON	DELI	
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No time window set.

Select

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Clear Selections

Restore Selections

Set Time Window

# **TecPlot-Ready Output**



# C2VSim ArcGIS Tool





# **Calibration Tools**





# **PEST-IWFM** Tools



# **PEST-IWFM Tools**

- Translate parameters from pilot points to IWFM
  - CVoverwrite.dat file
  - FAC2REALI program
- Convert IWFM hydrographs to SMP format
  - IWFM2OBS program
- Calculate vertical head differences to SMP format

   IWFM2OBS program
- Stream-groundwater flows to SMP format
  - STACDEP2OBS program
- Log-transform surface water hydrographs

   LOG\_TRAN\_SMP program

# **Documentation and User Support**

- Theoretical documentation, user's manual, reports, technical memorandums, previous presentations and posters, user's group presentations, and published articles in peer reviewed journals are available at the IWFM web site (google "IWFM")
- Technical support by DWR staff



# Validation and Verification

### Eleven verification runs; report available at IWFM web site (Ercan, 2006)

### VERIFICATION PROBLEMS FOR IWFM

#### This report is prepared under the direction of

Emin C. Dogrul, PhD, P.E., Tariq N. Kadir, P.E.

#### By

Ali Ercan

Department of Water Resources Bay-Delta Office Modeling Support Branch Hydrology and Operations Section

July 2006

	Test										
	1.a	1.b	1.c	1.d	2.a	2.b	3	4	5	6a	6b
Hydrological processes											
Groundwater flow											
Confined aquifer					氷	*			*		
Semi-confined aquifer							*				
Unconfined aquifer	*	*	*	*			*	*		*	*
Recharge/pumping wells											
Pumping					*	*	*		*		*
Recharge									*		*
Partially penetrating											
Multiple wells						非					
Tile drainage and											
subsurface irrigation											
Land subsidence									*		
Stream flows										*	*
Lakes											
Surface flows											
Soil moisture in the root											
zone											
and unsaturated zone											
Small watersheds											
Flow characteristics											
Steady state flow	*	*	*	*							
Transient flow					*	*	*	*	*	*	*
Boundary conditions											
Zero flow (impermeable	*	*	*	*	*	*	*	*	*	*	*
barrier)											
Specified flux		*									
Specified head	*				*	*	*	*		*	*
Rating table				*							
General head			*								
Dimensions											
1D	*	*	*	*				*			
2D					*	*	*		*	*	*
Quasi 3D											

## Validation of Z-Budget Post-processor

Z-Budget: Sub-Domain Water Budgeting Post-Processor for IWFM

Theoretical Documentation and User's Manual

Hydrology Development Unit Modeling Support Branch Bay-Delta Office February, 2010



#### Flow Computation and Mass Balance in Galerkin Finite-Element Groundwater Models

Emin C. Dogrul, P.E.1; and Tariq N. Kadir, P.E.2

Abstract: In most groundwater modeling studies, quantification of the flow rates at domain and subdomain boundaries is as important as the computation of the groundwater heads. The computation of these flow rates is not a trivial task when a finite-element method is chosen to solve the groundwater qualton. Generally, it is believed that finite-element methods do not conserve runss locally. In this paper, a postprocessing technique is developed to compute mass-conserving flow rates at element faces. It postprocesses the groundwater head field obtained by the Gadewise finite-element method, and the calculated flow rates conserve mass locally and globally. The only requirement for the postprocessor to be applicable is the irrotationality of the flow field, i.e., the curf of the Darcy flow should be zero. The accuracy and the mass conservation properties of the new postprocessor are demonstrated using several test problems that include one-, two, and three-dimensional flow systems in both homogeneous and feterogeneous aquifer conditions.

DOI: 10.1061/(ASCE)0733-9429(2006)132:11(1206)

CE Database subject headings: Finite element method; Mass: Ground-water flow: Computer analysis: Computation; Hydrologic models.

#### Introduction

Finite-element methods, particularly the Galerkin finite-element method (GFEM), are commonly utilized in groundwater modeling studies because complex boundaries can be represented more closely. Generally, the momentum equation, i.e., Darcy equation, is substituted into the equation of mass conservation, and the resulting equation is solved for the groundwater head. In most groundwater modeling studies, quantification of flow rates is as important as the simulation of the groundwater heads. One reason for this is that most groundwater basins are divided into political subdomains such as water districts, counties, or states with differing strategies of managing their groundwater resources. Simulation of groundwater flow rates between adjacent subdomains caused by varying management strategies is sometimes the ultimate goal of a modeling study. Another reason is the need to examine the detailed inflow/outflow components at a subdomain level during calibration and verification stages of a modeling study

When the flow rates are required, the conventional approach is to postprocess the groundwater head field, computed using GFEM, by substituting it into the Darcy equation and obtaining

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Note. Discussion open until April 1, 2007. Separate discussions most is solvenited for indrividual papers. To extend the closing data by one month, a vvitten request must he filed with the ASCE Managing Editor. The manuscript for this paper vas submitted for review and possible publication on March 15, 2005; approved on December 20, 2005. This paper is part of the Journal of Hysterulic Engineering, Vol. 132, No. 11, November 1, 2006. ©ASCE, ISSN 0735-9429/2006/11-1206–1214/ \$255.00.

1206 / JOURNAL OF HYDRAULIC ENGINEERING @ ASCE / NOVEMBER 2006

the flux field. Then, the normal component of the Darcy flux is integrated over the domain or subdomain boundary to obtain the flow rates. However, this postprocessing approach has been shown to generate flow rates that violate local as well as global mass balances. Yeh (1981) reported global mass balance errors of up to 30% when the conventional postprocessing method is used. He suggested that the finite-element approach that is used to simulate the groundwater head field also be applied to Darcy equation with the fluxes as the state variables. Although his method produced better results, test problems still showed mass balance errors of 2-9% (Yeh 1981). Commenting on Yeh's work, Lynch (1984) showed that precise global mass balance can be achieved in GFEM by proper treatment of the Dirichlet boundary conditions. He pointed out that the common practice of discarding Galerkin equations-the discrete version of the conservation equation-along Dirichlet boundaries violates the mass balance by requiring that these fluxes he approximated by the conventional postprocessing method. He showed that retaining the Galerkin equation at Dirichlet boundaries as the equation for the flux resulted in precise global mass balance. Similar observations have been made by other researchers (Carey 1982; Carey et al. 1985; Hughes et al. 2000: Berger and Howington 2002: Carey 2002). In fact, the same idea can be used to compute the internal fluxes, i.e. once the groundwater head at an internal node is committed with GFEM, that node can be treated as a Dirichlet boundary and the Gaterkin equation at the node can be solved for the flux (Hughes et al. 2000; Carey 2002). Cordes and Kinzelbach (1992) used an alternative postprocessing method where the elements were subdivided into patches and individual fluxes for each patch were computed by assuming that the flow field was irrotational. In their method, triangular and quadrilateral elements were treated separately.

The aim of this paper is to develop and test a postprocessor that uses the groundwater beads computed by GFEM to obtain flow rates across finite-element faces, i.e., normal flux integrated along each of the element faces, that do not violate local and global mass balances. Once flow rates through each of the ele-

# **Key Limitations**

- Time step and stream routing: Stream flow must travel from upstream to downstream within the length of time step for the zero-storage assumption to be valid
- Time step and rainfall runoff: Re-calibrate curve numbers for different time steps (for C2VSim, the input data time step is itself a limitation)
- Spatial scale of demand and supply: Demand and supply computations are performed at the subregion level
- Vertical distribution of pumping: Static distribution limits the ability to simulate changes in the pumping depth during simulation period
- Aquifer and root zone thickness: Aquifer thickness should be large
  compared to root zone thickness to minimize error in case groundwater
  table is close to ground surface; likely to occur in native and riparian
  vegetation areas

# **IWFM Development**

- Version 3.02:
  - Subregion water budgets
- Version 4
  - Element water budgets

# New Features of IWFM v4

- Improved root zone module (a.k.a. IDC v4)
  - Root zone flow processes and agricultural water demands are computed at each cell for each land-use type
  - Agricultural water demands are computed using methods from irrigation scheduling models
  - Explicit simulation of rice and refuge operations
  - Simulation of re-use of agricultural tail water at different spatial resolutions
  - Simulation of regulated deficit irrigation
  - Ability to specify water demands (i.e. contractual demands) instead of computing them dynamically
  - Explicit representation of effective precipitation and ETAW
  - Detailed budget output for each land-use type

# New Features of IWFM v4

- Ability to run the root zone module (IDC) by itself or as linked to IWFM with the same input data files
- Reduced size of Z-Budget binary output file for run-time efficiency
- Water budget output at user-selected stream nodes
- Ability to generate water budget tables accumulated to time steps larger than the simulation time step
## Future IWFM Developments

- Improved simulation of riparian vegetation
- Improved simulation of rainfall-runoff and overland flow
- Improved hydraulic routing of stream flows that account for change in storage
- Continue developing ArcGIS based GUI
- Simulation of water quality
- Emulate an agricultural economics model in IWFM
- Parallel processing

## **IWFM Applications**

- California Central Valley Groundwater-Surface Water Model
- Butte County Groundwater Model (Heywood, CDM)
- Walla Walla River Basin Model (Petrides, OSU)
- Yolo County Integrated Model (DWR, UCD)
- Kings River Model (HydroMetrics)
- Merced Area (MAGPI, RMC)

## END

