

# Black Butte Dam Erosion Repairs

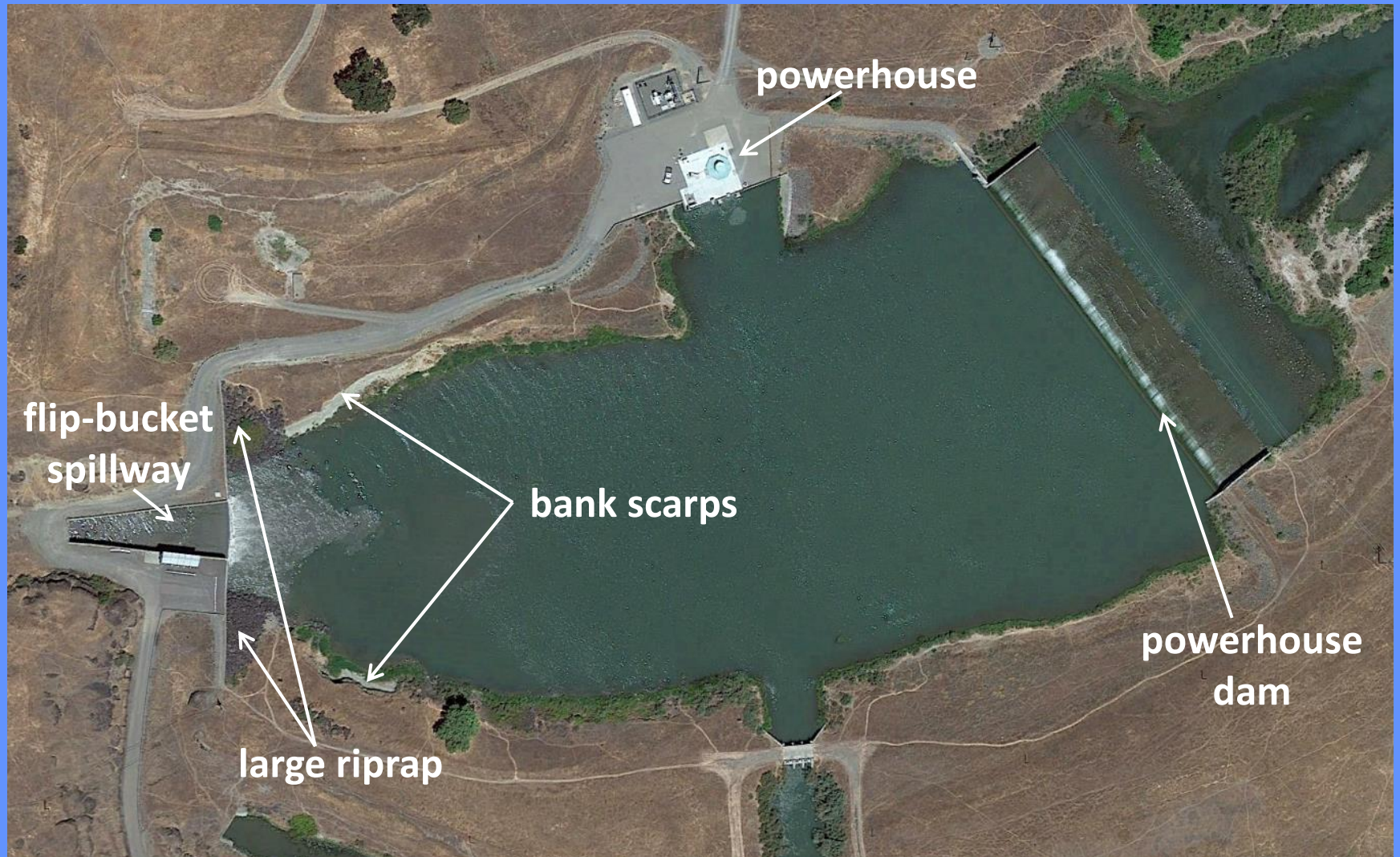
3D Model and Analysis

April 12, 2016

Will L'Hommedieu



# Site Overview



# North Bank Scarp




# What is a flip-bucket?



VIZIO

# What is a flip-bucket?



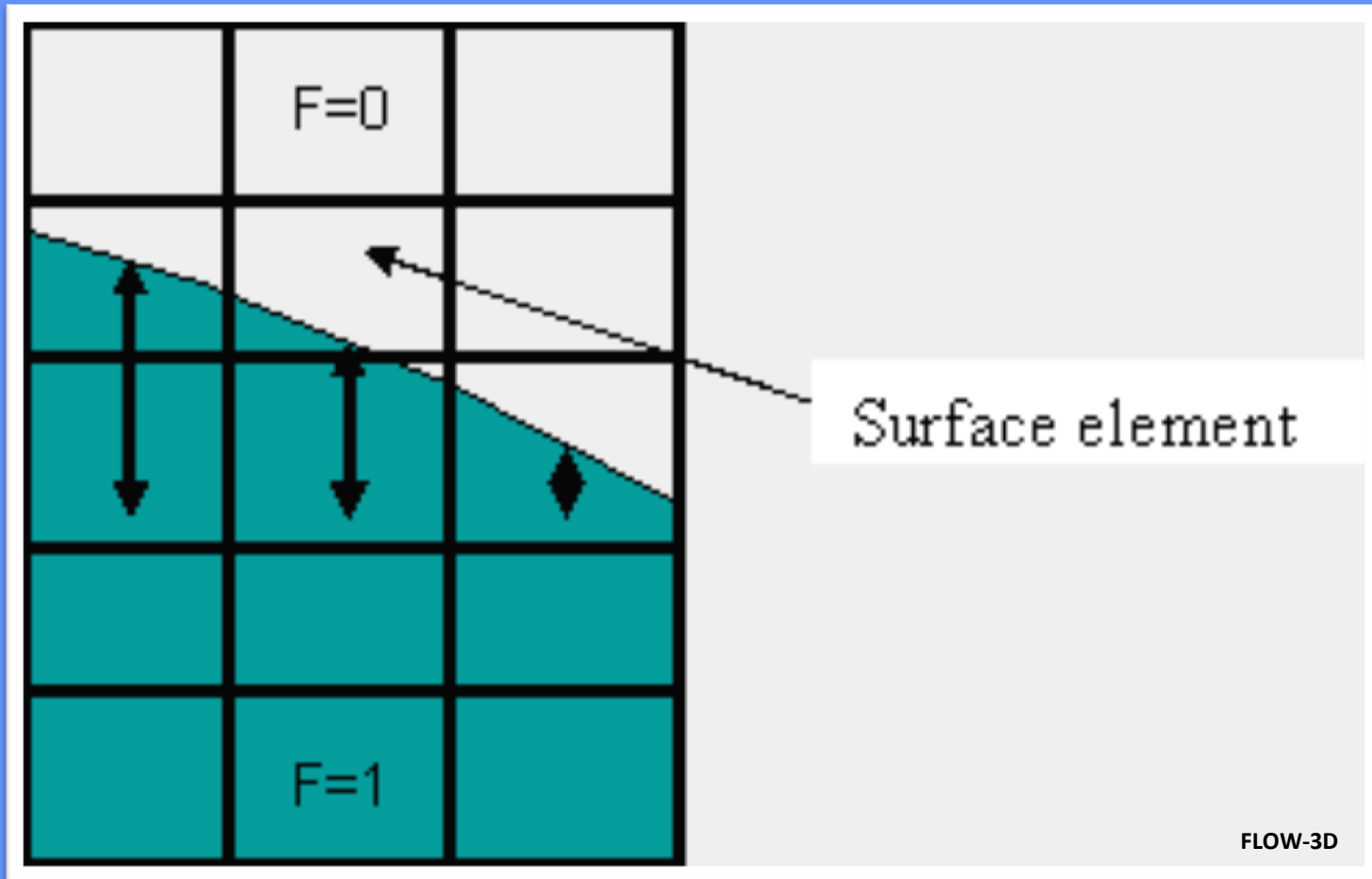
15000 CFS  
1.21.93

U1210

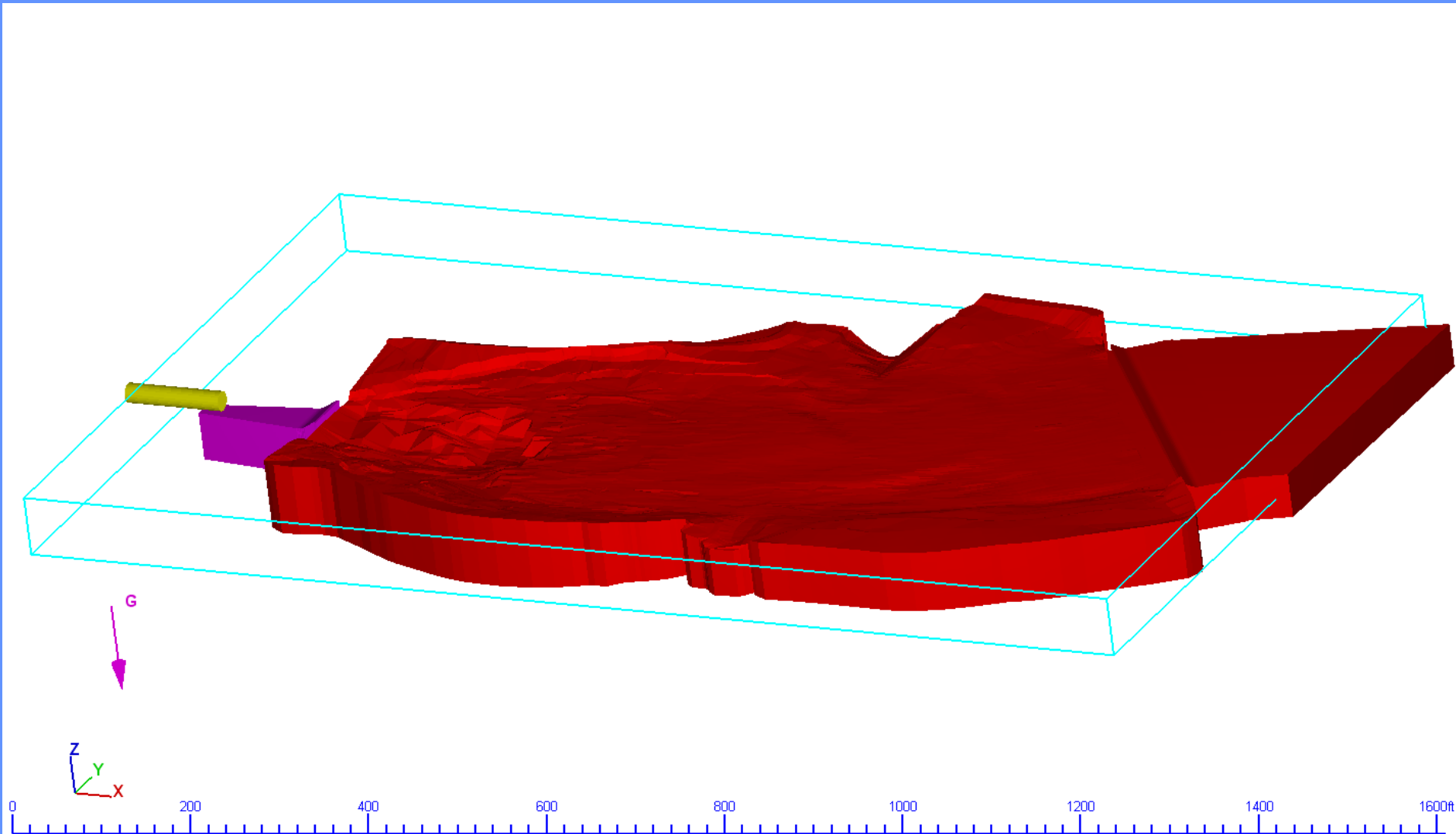
# FLOW-3D

## VOF

(Volume of Fluid)

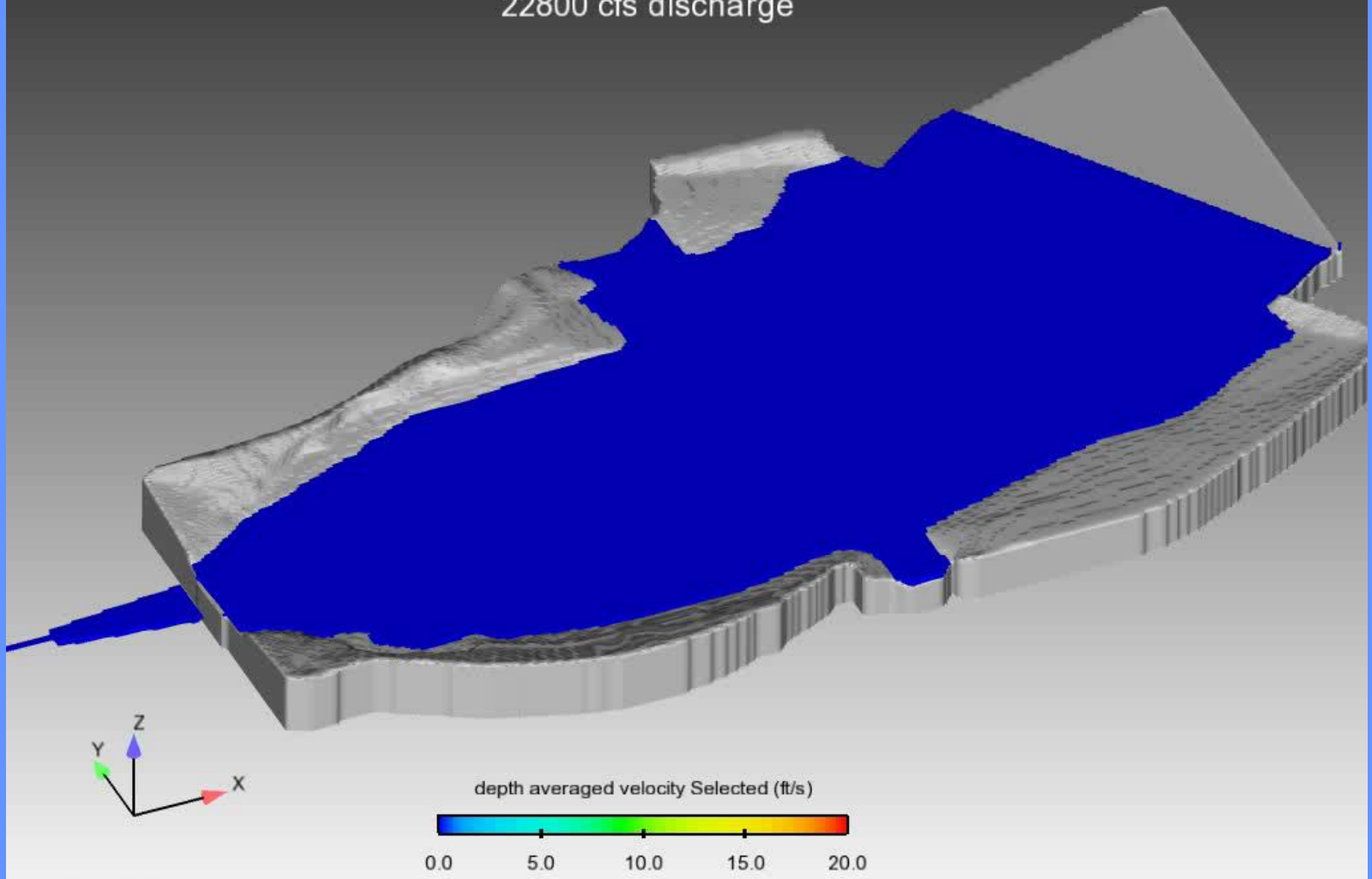


# Model Geometry



# Simulation Results

CBEC Bucket Spillway Discharge Analysis  
22800 cfs discharge

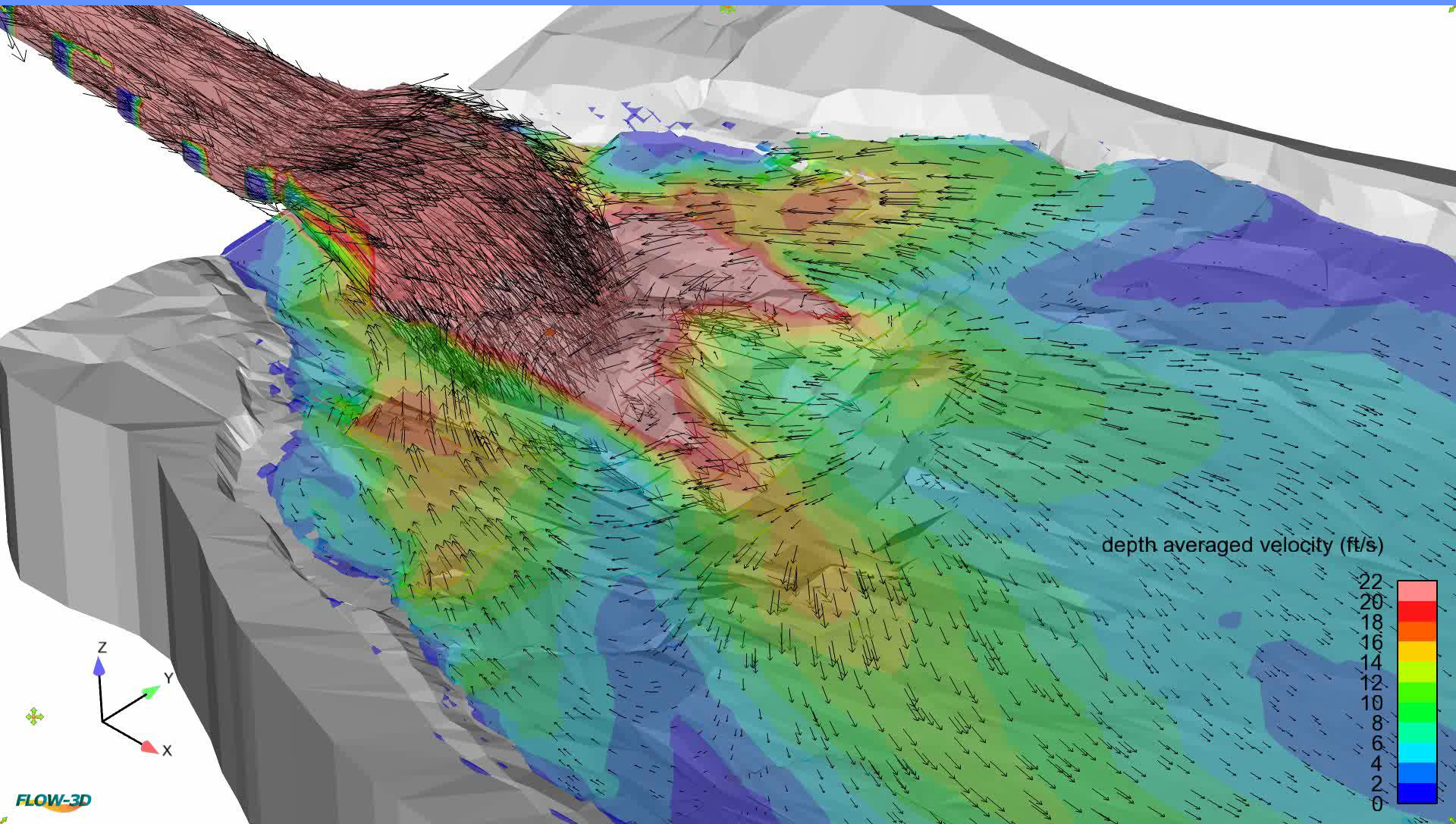


**FLOW-3D**

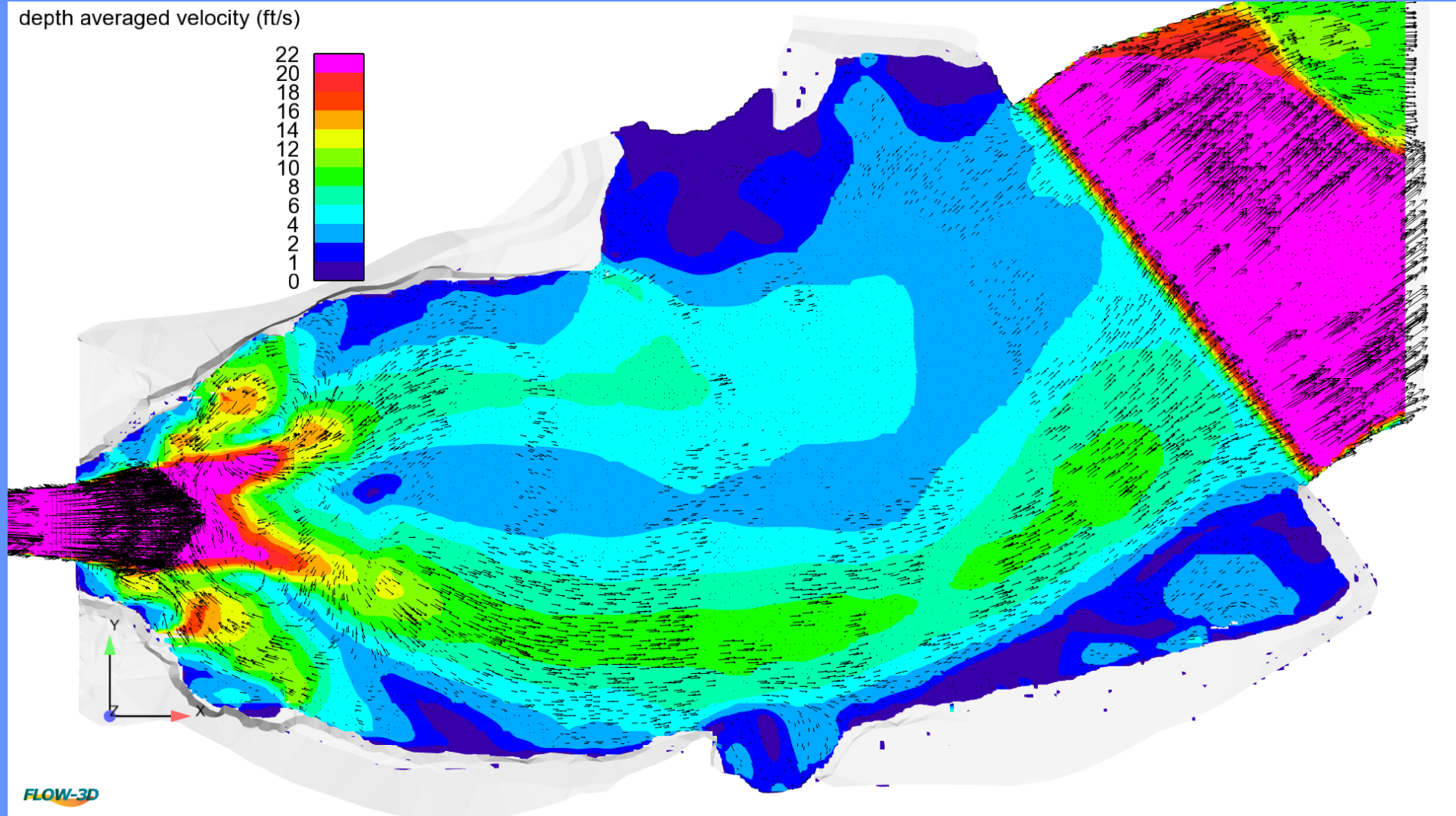
Time = 0s



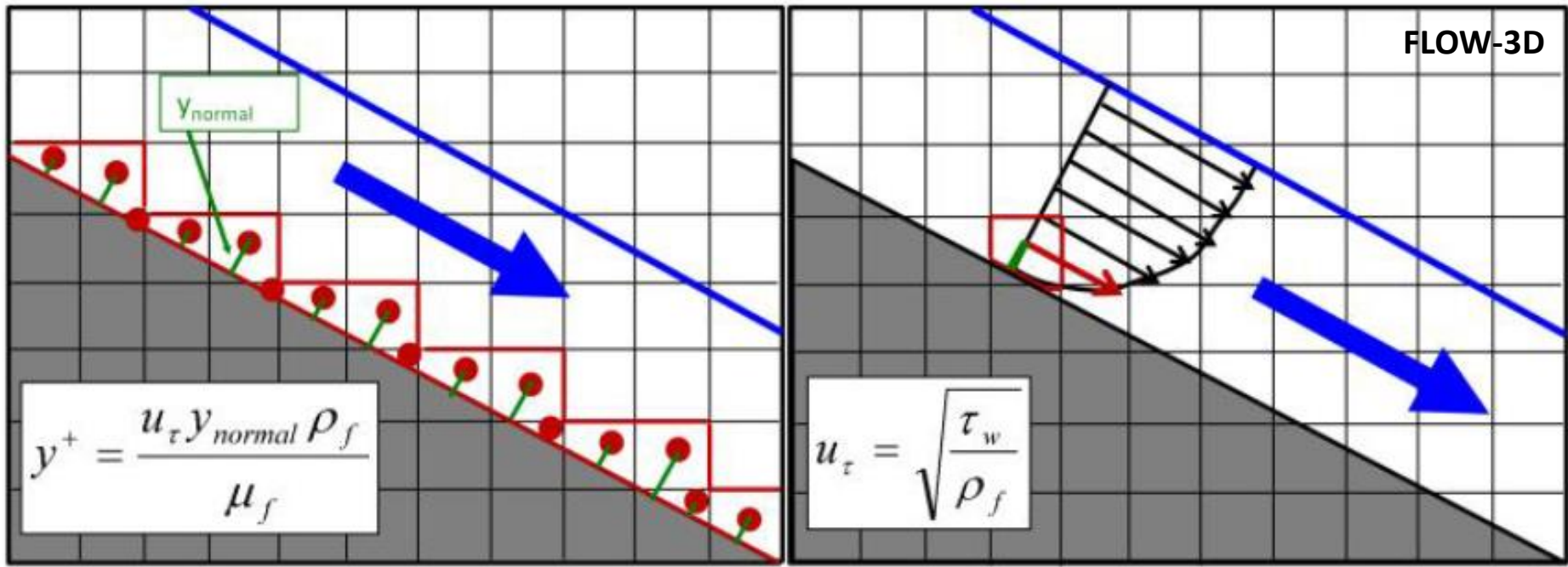
# Simulation Results



# Simulation Results



# Challenge #1: Mesh Resolution



**Solution:** use depth averaged velocity with coarse model resolution

# Challenge #2: Which equation is right for me?

Need to size riprap to resist erosion:

## 1. Eddies

- a) **Shear Stress** – Shield's Equation w/ bed shear stress from depth averaged velocity
- b) **Empirical** – USACE and HEC-11 velocity based

## 2. Waves

- a) **Empirical** – USACE and HEC-11 wave-height based

# Challenge #2a: How do we calculate Cd?

- In order to calculate bed shear we need to have drag coefficient

$$\tau_b = \rho C_d \bar{v}^2$$

$$d_{50} = \frac{\tau_b}{\tau^* (\gamma_s - \gamma_w)}$$

- Large depth range

- FLOW-3D sediment transport  $C_d = f(d, K_s)$

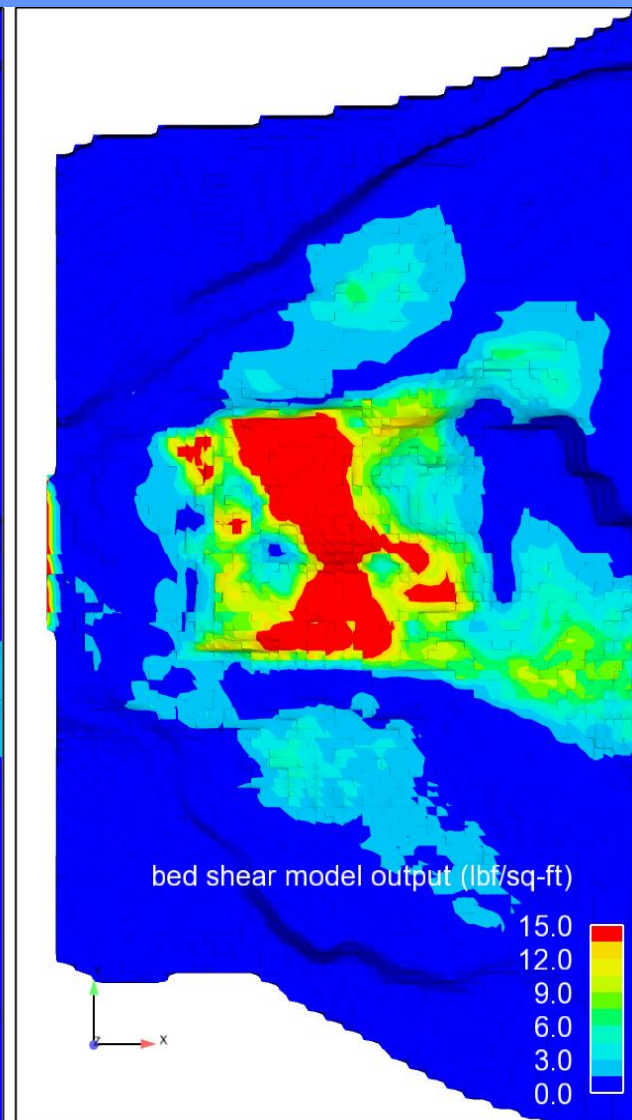
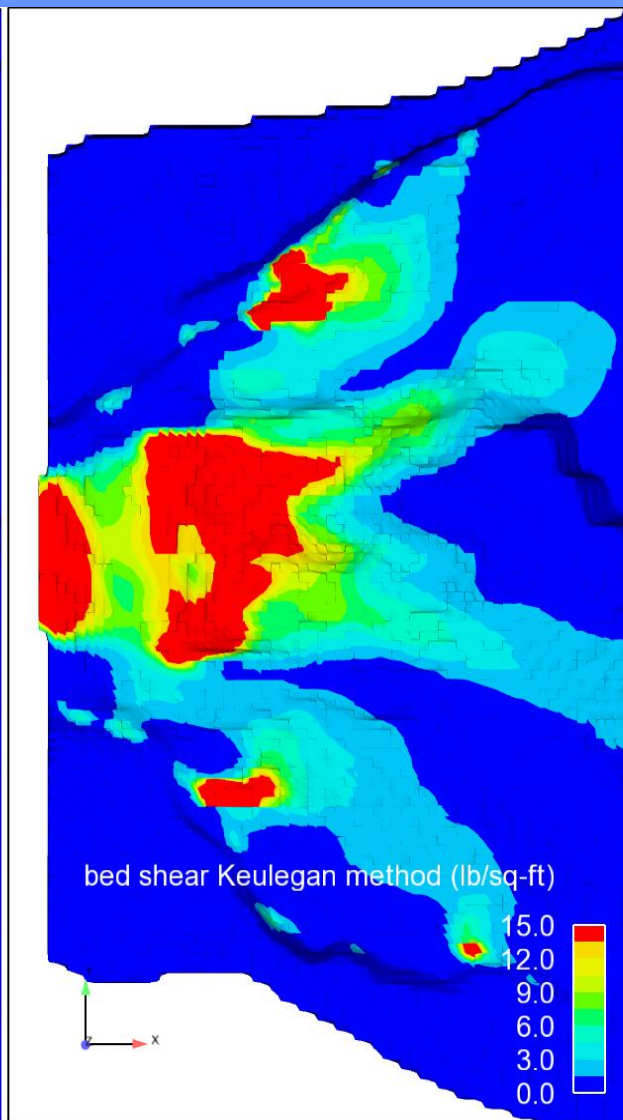
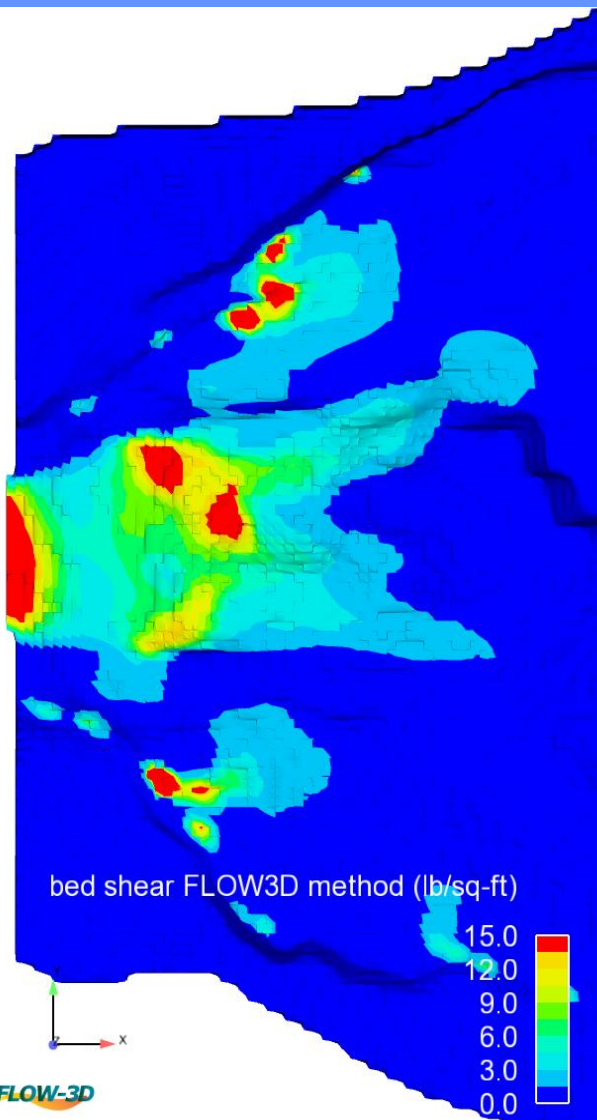
$$C_d = \left( \frac{k}{\beta + \ln \left( \frac{k_s/30}{h} \right)} \right)^2$$

- Keulegan equation  $C_d = f(d, K_s, F)$

$$C = 32.6 * \log_{10} \left[ 10^{\frac{A_r \sqrt{g}}{32.6}} \frac{R}{k_s} \right] \quad n = \frac{1.486}{C} R^{1/6} \quad C_d = g \frac{n^2}{h^{1/3}}$$

- Both **fail** at low depth to substrate height ratios

# Bed Shear – Comparison



## Challenge #2b Safety/Adjustment Factors

- Empirical equations developed to calculate rock size using 1D model results of main channel depth and velocity
- We used a 3D model so we should have much more accurate near bank values

**HEC-11**

$$d_{50} = C_{sg}C_{sf} \frac{0.001V^3}{h^{1/2}k_1^{3/2}}$$

**USACE**

$$d_{30} = S_f C_s C_v C_t d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \frac{V}{\sqrt{k_1 g d}} \right]^{5/2}$$

## Challenge #2c: Waves

- Model likely not turbulent enough to fully characterize standing waves
  - To capture standing waves need LES
- **Solution**: estimated wave height and period from video and corroborate with model observations

rock size

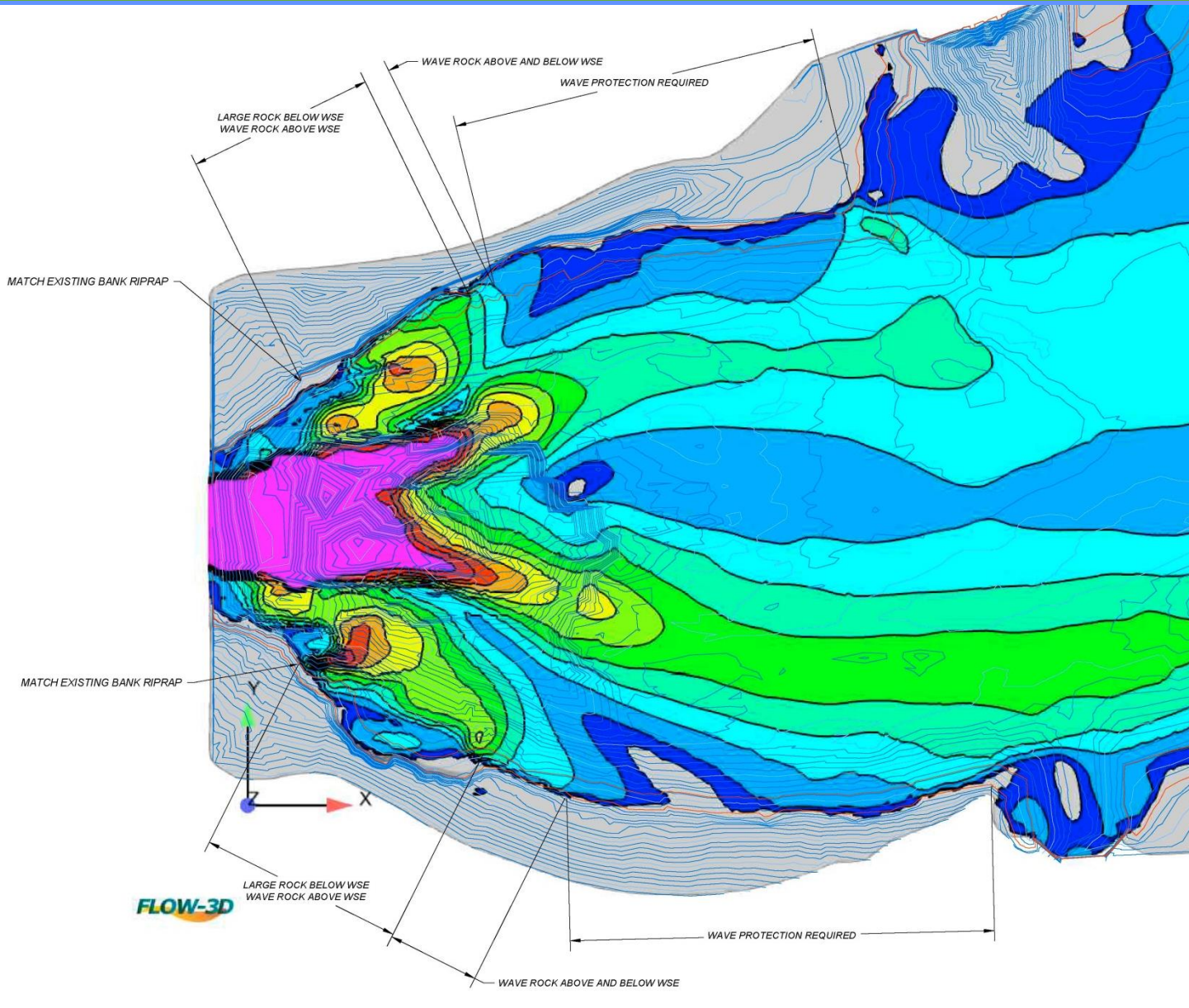
$$W_{50} = \frac{H^3 \gamma_r}{k_D \left( \frac{\gamma_r}{\gamma_w} - 1 \right)^3 \cot \theta} \longrightarrow d_{50} = \left( \frac{6W_{50}}{\gamma_r \pi} \right)^{1/3}$$

run up height

$$\varepsilon = \frac{\tan \theta}{\left( \frac{2\pi H}{gT_p^2} \right)^{1/2}} \longrightarrow R_{max} = H * \frac{a\varepsilon}{1 + b\varepsilon}$$



# Rock Recommendations

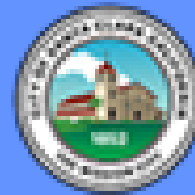


# Riprap Size Comparison

Method	Average D50 Absolute (ft)	Average D50 Relative
FLOW-3D Cd - Shear	1.0	0.6
HEC-11 - Wave	1.4	0.8
<b>USACE - Wave</b>	<b>1.7</b>	<b>0.9</b>
Model Output – Shear*	1.8	1.0
Keulegan Cd - Shear	2.4	1.3
HEC-11 - Velocity	3.3	1.9
<b>USACE - Velocity</b>	<b>3.4</b>	<b>1.9</b>

# Acknowledgments

- Sam Diaz (cbec eco engineering)
- Matt Powers (GEI Consultants)
- City of Santa Clara



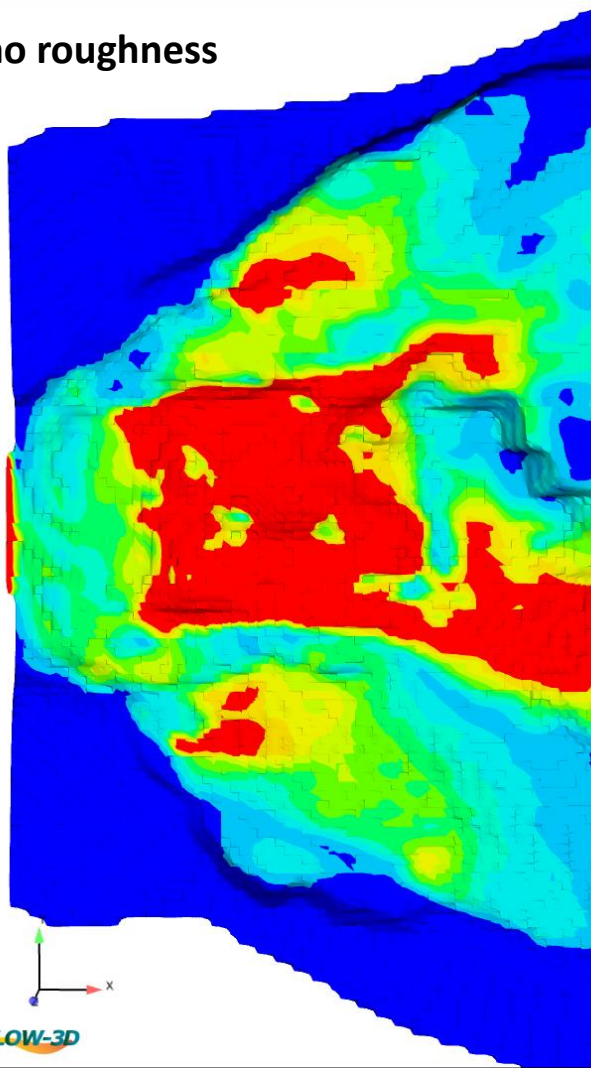
**City of  
Santa Clara**  
*The Center of What's Possible*

# Questions?

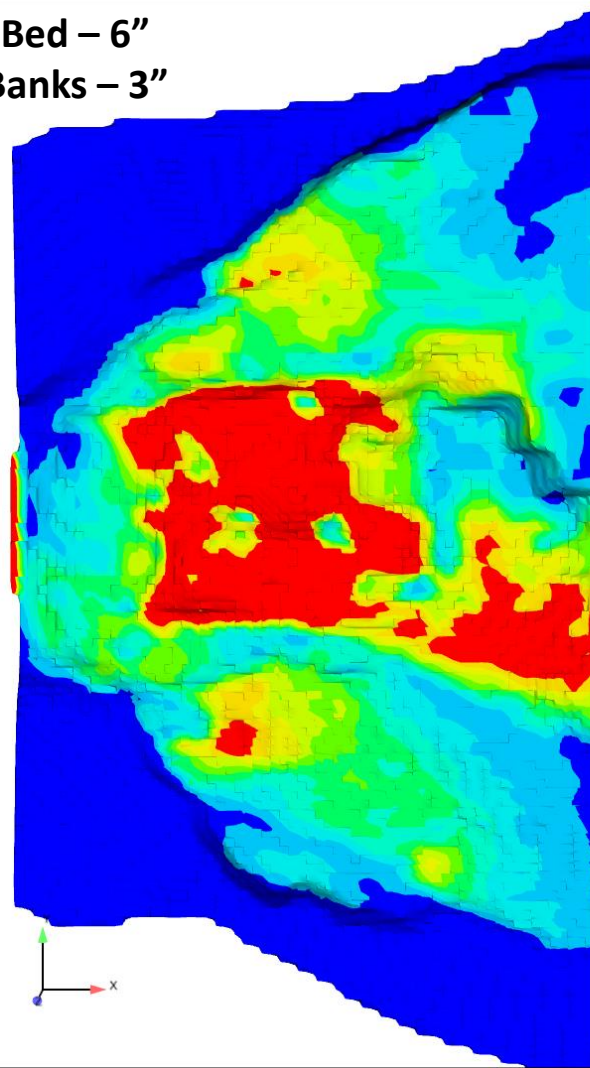


# Roughness Sensitivity Testing

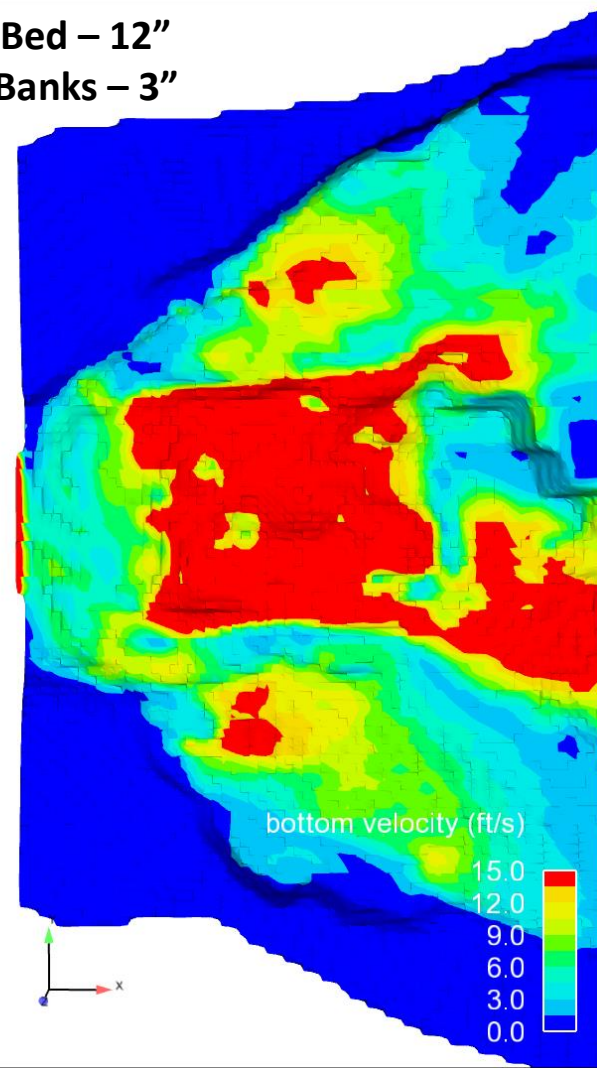
no roughness



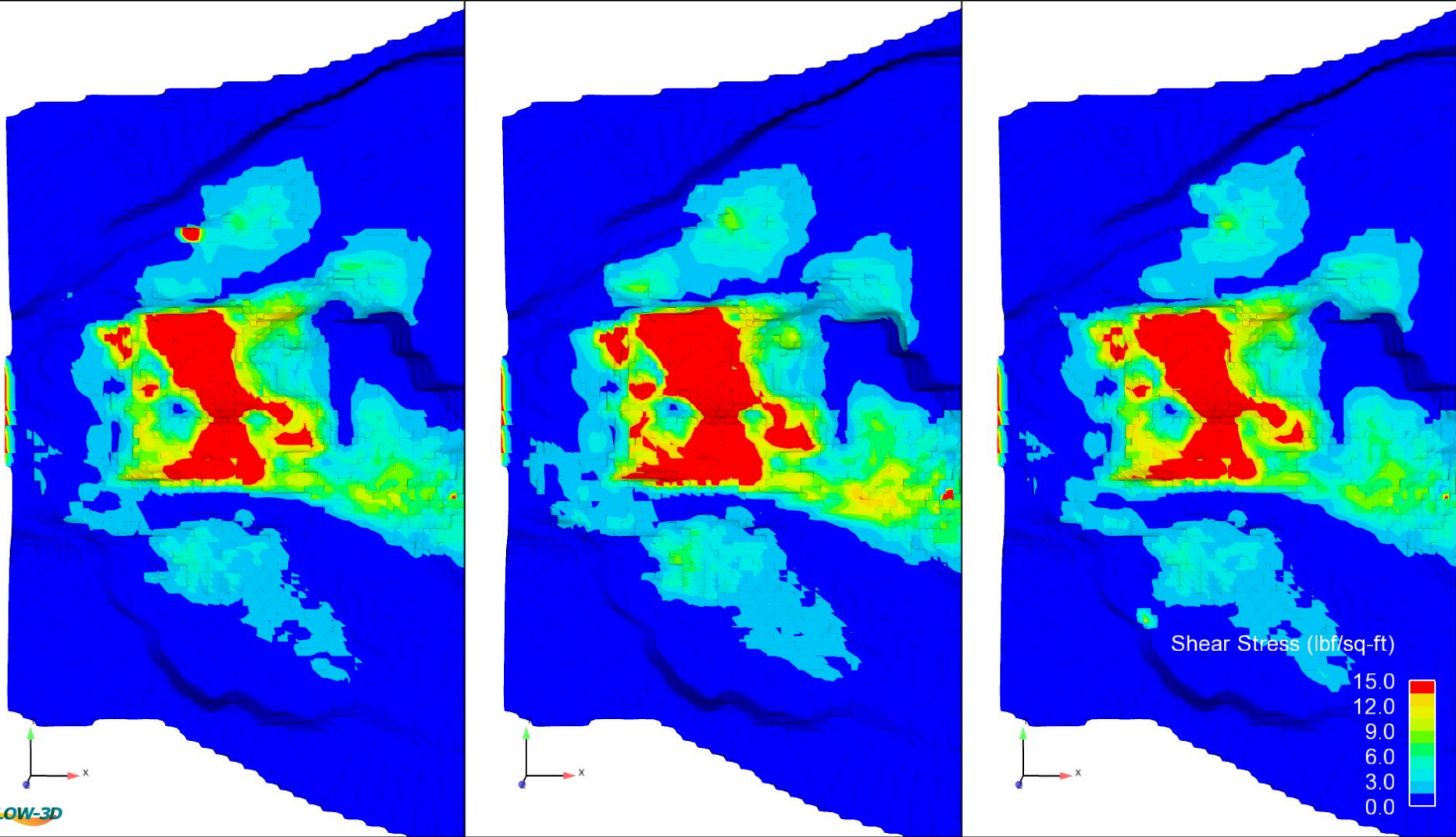
Bed – 6"  
Banks – 3"



Bed – 12"  
Banks – 3"



# Roughness Sensitivity Testing



# Picking Representative Values

