

Stream-Aquifer
seepage estimation
*with a simple analytic
algebraic tool*

by the team of
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Motivation for study

As an example, in a study for the Santa Rosa Plain Watershed Groundwater Management Plan, the horizontal square grid size is 660 feet and the area under investigation is 262 square miles. None of the rivers in the area have widths that exceed 100 feet. **Thus all river reaches are included in cells that have dimensions far in excess of the river widths.** The water table aquifer that always exceeds 90 feet of thickness is **treated as a single calculation layer in the vertical direction.**

In such context the **boundary condition** to determine the seepage discharge is chosen to be of the **third type**. The discharge is calculated as being proportional to the difference between the head in the river, h_S , and the head in the aquifer, h_a , **at the center of the vertical thickness of the cell that contains the river.** The proportionality coefficient depends upon (1) the length of the river reach, L , within the cell that includes it (the river cell), (2) the hydraulic conductivity of the aquifer in the vicinity of the river, K , and (3) that chosen distance where aquifer head, h_a , is calculated from the overall domain calculation matrix. Symbolically the relation is:

$$Q = \kappa KL(h_S - h_a) = C_{riv}(h_S - h_a) \quad (1)$$

In most groundwater models used commercially, the determination of the coefficient C_{riv} is pretty much left to the user and most often determined by calibration when historical data are available.

Thus the need for a more rigorous estimation of that coefficient.

Slightly penetrating river

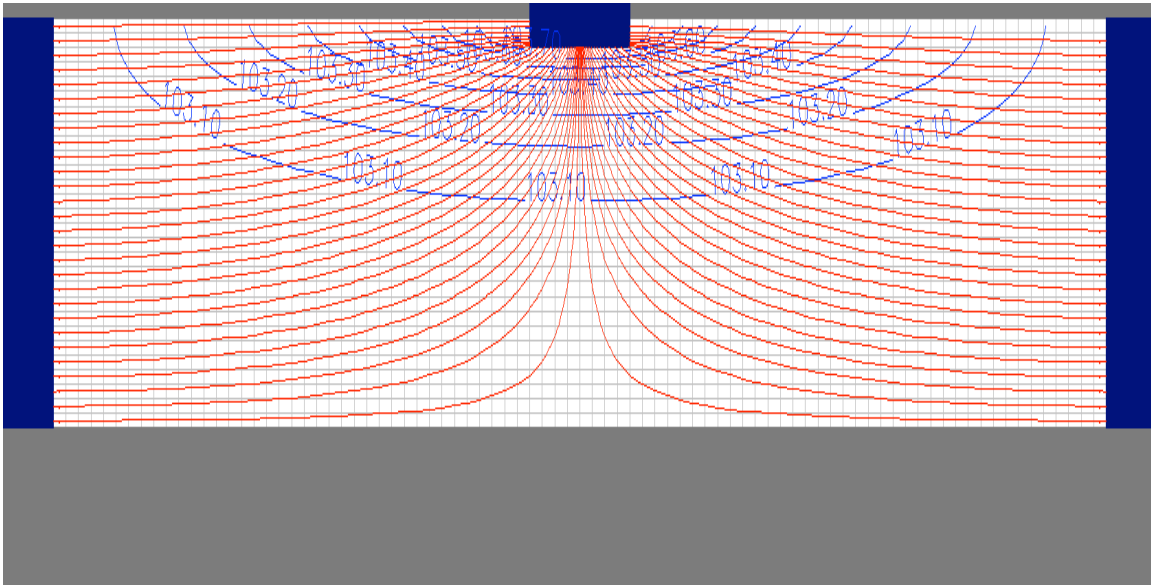
(Figure not to scale)

Same parameters as for the isotropic case

Anisotropic condition

Anisotropy ratio, $RANIS = K_V / K_H = 0.01$

Reduction factor = 0.204



$$Q_{anis} = R_f(\xi)Q_{iso}$$

$$\xi = (1 - DOP)(1 - \sqrt{RANIS})$$

DOP = Mean depth of penetration/aquifer thickness

$$R_f = 1.00064 - 0.395577\xi - 0.647687\xi^2$$

Derivation of formulae

Case of isotropy

For the case of elliptical, rectangular and trapezoidal river cross-sections the results were obtained exactly analytically and verified with very refined grids in numerical models such as MODFLOW.

(see bibliography)

If the wetted perimeter and the degree of penetration are the same, the shape of the cross-section has practically no impact on the value of Γ_{iso} , the SAFE (Stream-Aquifer Flow Exchange) dimensionless conductance

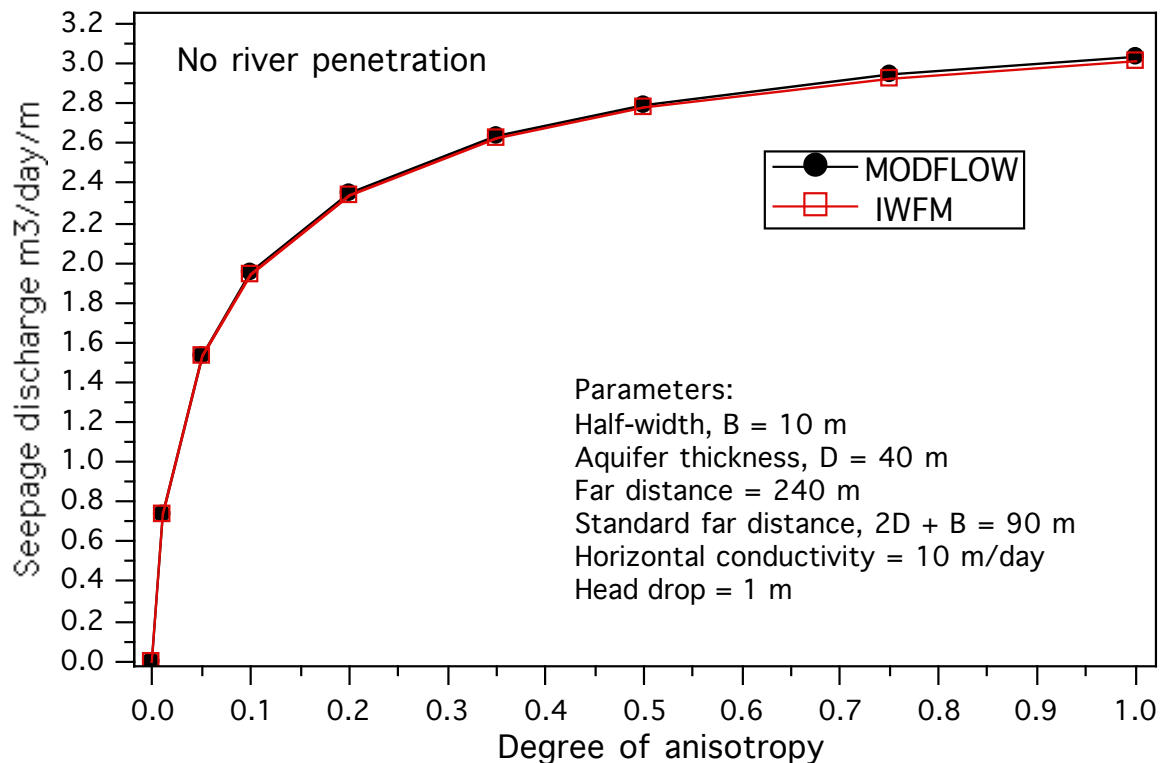
Derivation of formulae

Case of anisotropy

Again the results were obtained exactly analytically and numerically and verified with very refined grids in widely used numerical models such as MODFLOW, IWFM and ASMWIN.
(see attached bibliography)

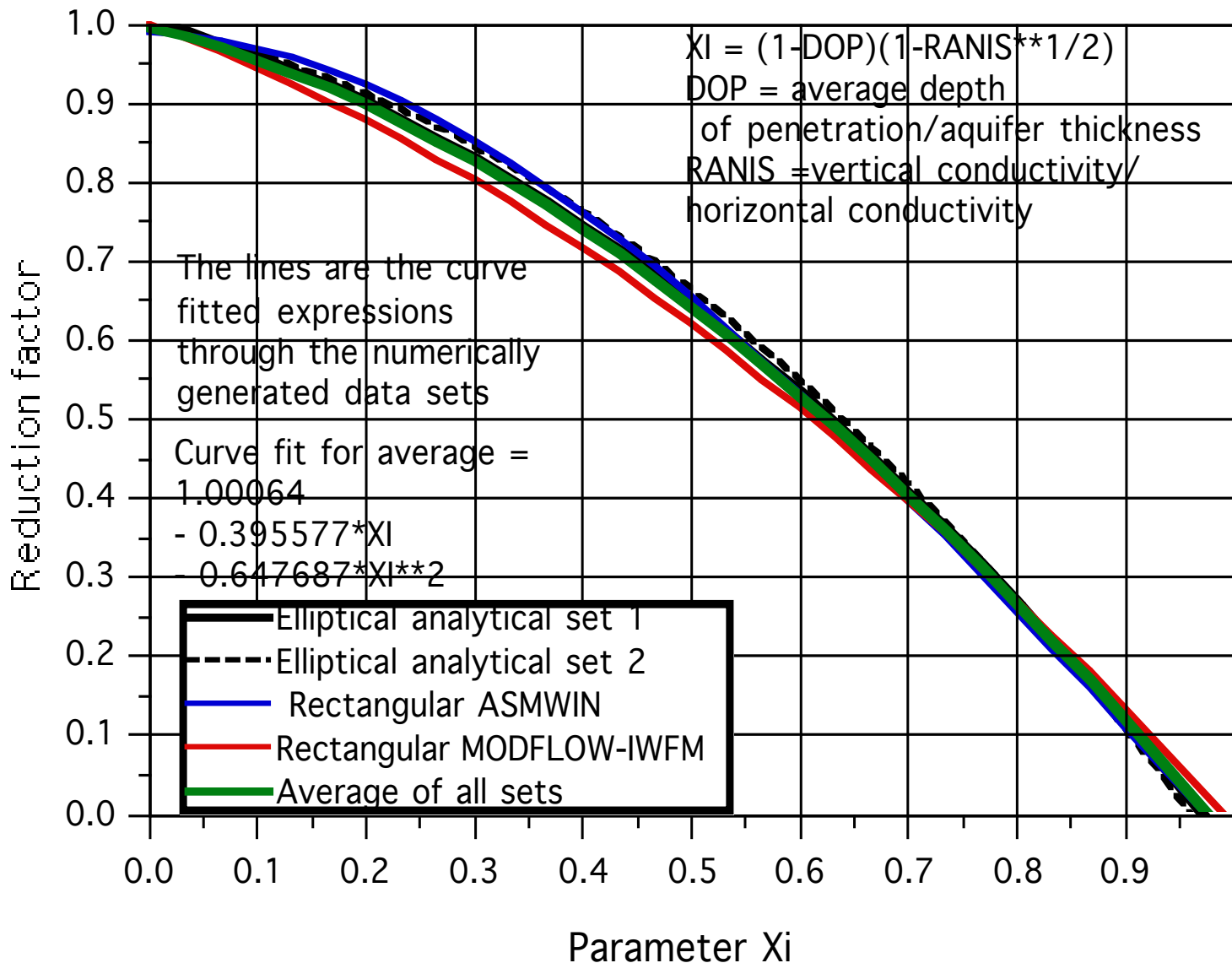
Independent runs by
MODFLOW and IWFM with
the same refined grid scheme
for a rectangular cross –
section gave essentially
identical results.

Comparison of results by MODFLOW and IWFM



Comparison of Reduction factor for elliptical and rectangular cross sections. The river cross-section shapes have little influence on the river seepage as long as the wetted perimeter and the degree of penetration are the same. This figure applies for the constant head boundary condition prescribed at a far distance **twice** the aquifer thickness away from the river bank.

Reduction factor as function of anisotropy and degree of penetration



Advantages

The research has led to the estimation of the seepage discharge **accounting** for

- (1) the wetted perimeter,
- (2) the degree of penetration,
- (2) a clogging layer,
- (4) aquifer anisotropy, and
- (5) location of the far distance.

It eliminates the burden of **numerous numerical calculations** while maintaining a **superior accuracy**

Conclusion

Having investigated all the factors that influence seepage it remained to show how to incorporate the new approach into models like MODFLOW for estimating the coefficient “ C_{riv} ” without any change to MODFLOW’s code.

In the bibliography see item (5) and if interested enter your name and email address in the sign-up sheet.

$$C_{riv} = 2GK_H \left\{ \frac{\Gamma_{anis-\Delta-rcl}}{1 - \left(\frac{G}{D}\right)\Gamma_{anis-\Delta-rcl}} \right\}$$

G : grid size i.e. side length of horizontal square cell

$\Gamma_{anis-\Delta-rcl}$: SAFE dimensionless conductance associated with a level of anisotropy, an excess far distance over the natural standard far distance for that anisotropy ratio and a real clogging layer

$$\Delta = G - xfar_{anis-standard}$$

$xfar_{anis-standard}$: natural standard far distance for that anisotropy ratio

D : aquifer thickness

K_H : horizontal aquifer conductivity

(1) Morel-Seytoux, H.J. (2009), The turning factor in the estimation of stream-aquifer seepage, *Ground Water*, 47, 205-212, doi: 10.1111/j.1745-6584.2008.00512.x.

(2) Miracapillo, C., and H. J. Morel-Seytoux. (2014), Analytical solutions for stream-aquifer flow exchange under varying head asymmetry and river penetration: Comparison to numerical solutions and use in regional groundwater models, *Water Resour. Res.*, 50, doi:10.1002/2014WR015456.

(3) Miracapillo, C., Steffen Mehl and H. J. Morel-Seytoux. (2016). Stream-Aquifer Flow Exchange dimensionless conductance under conditions of anisotropy. Submitted January 26, 2016 to *Groundwater Journal*. Under review.

(4) Morel-Seytoux, H.J., Steffen Mehl and Kyle Morgado. (2013), Factors influencing the stream-aquifer flow exchange coefficient, *Ground Water*, 49(5): 775-781. doi: 10.1111/gwat.12112, 7 pages.

(5) Morel-Seytoux, H.J., Calvin Miller, Steffen Mehl and Cinzia Miracapillo, (March 2016). River seepage conductance in large-scale regional studies. Draft in final stage of preparation.

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